# **GAS MIXTURES**

- 1. Composition of a Gas Mixture
  - Mass and Mole Fractions
- 2. P-v-T Behavior of Gas Mixtures
  - Ideal and Real Gases
- **3.** Properties of Gas Mixtures (u<sub>m</sub>, h<sub>m</sub>, s<sub>m</sub>, etc)
  - Ideal and Real Gases



**CHAPTER** 

## **Objectives**



- Develop rules for determining nonreacting gas mixture properties from knowledge of mixture composition and the properties of the individual components.
- Define the quantities used to describe the composition of a mixture, such as mass fraction, mole fraction, and volume fraction.
- Apply the rules for determining mixture properties to idealgas mixtures and real-gas mixtures.
- Predict the *P*-*v*-*T* behavior of gas mixtures based on Dalton's law of additive pressures and Amagat's law of additive volumes.







To determine the properties of a mixture, we need to know the *composition* of the mixture as well as the properties of the individual components. There are two ways to describe the composition of a mixture:

Molar analysis: specifying the number of moles of each component

Gravimetric analysis: specifying the mass of each component

$$m_m = \sum_{i=1}^k m_i$$
 and  $N_m = \sum_{i=1}^k N_i$  (13-1a, b)

$$mf_{i} = \frac{m_{i}}{m_{m}} \text{ and } y_{i} = \frac{N_{i}}{N_{m}}$$
Mass Mole
fraction fraction

(13-2a, b)









#### FIGURE 13-1

The mass of a mixture is equal to the sum of the masses of its components.



#### FIGURE 13-2

The number of moles of a nonreacting mixture is equal to the sum of the number of moles of its components.







$$\sum_{i=1}^{k} \text{mf}_i = 1$$
 and  $\sum_{i=1}^{k} y_i = 1$ 

The sum of the mass and mole fractions of a mixture is equal to 1.

$$H_{2} + O_{2}$$

$$y_{H_{2}} = 0.75$$

$$y_{O_{2}} = \frac{0.25}{1.00}$$

#### FIGURE 13-3

The sum of the mole fractions of a mixture is equal to 1.







$$M_{m} = \frac{m_{m}}{N_{m}} = \frac{\sum m_{i}}{N_{m}} = \frac{\sum N_{i}M_{i}}{N_{m}} = \sum_{i=1}^{k} y_{i}M_{i}$$

Apparent (or average) molar mass

m = NM

$$R_m = rac{R_u}{M_m}$$
 Gas (13-3a, b)

$$M_m = \frac{m_m}{N_m} = \frac{m_m}{\sum m_i/M_i} = \frac{1}{\sum m_i/(m_m M_i)} = \frac{1}{\sum_{i=1}^k \frac{\mathrm{mf}_i}{M_i}}$$
 The molar mass of a mixture

$$\mathrm{mf}_i = \frac{m_i}{m_m} = \frac{N_i M_i}{N_m M_m} = y_i \frac{M_i}{M_m}$$

Relation between mass (13-5)and mole fractions of a mixture









#### FIGURE 13–5

Dalton's law of additive pressures for a mixture of two ideal gases.



#### FIGURE 13-6

Amagat's law of additive volumes for a mixture of two ideal gases.

The prediction of the *P*-*v*-*T* behavior of gas mixtures is usually based on two models:

#### Dalton's law of additive

pressures: The pressure of a gas mixture is equal to the sum of the pressures each gas would exert if it existed alone at the mixture temperature and volume.

#### Amagat's law of additive

volumes: The volume of a gas mixture is equal to the sum of the volumes each gas would occupy if it existed alone at the mixture

temperature and pressure.







Dalton's law: (13-6)

Amagat's law: (13-7)  $P_{m} = \sum_{i=1}^{k} P_{i}(T_{m}, V_{m}) \begin{cases} \text{exact for ideal gases,} \\ \text{approximate} \end{cases}$   $V_{m} = \sum_{i=1}^{k} V_{i}(T_{m}, P_{m}) \begin{cases} \text{for real gases} \end{cases}$ 

 $P_i$  component pressure V<sub>i</sub> component volume  $P_i / P_m$  pressure fraction  $V_i / V_m$  volume fraction

For ideal gases, Dalton's and Amagad's laws are identical and give identical results.



#### FIGURE 13–7

The volume a component would occupy if it existed alone at the mixture T and P is called the *component volume* (for ideal gases, it is equal to the partial volume  $y_i V_m$ ).







#### **Ideal-Gas Mixtures**



This equation is only valid for ideal-gas mixtures as it is derived by assuming idealgas behavior for the gas mixture and each of its components.

The quantity  $y_i P_m$  is called the **partial pressure** (identical to the *component pressure* for ideal gases), and the quantity  $y_i V_m$  is called the **partial volume** (identical to the *component volume* for ideal gases).

Note that for an ideal-gas mixture, the mole fraction, the pressure fraction, and the volume fraction of a component are identical.

The composition of an ideal-gas mixture (such as the exhaust gases leaving a combustion chamber) is frequently determined by a volumetric analysis (Orsat Analysis).







#### **Real-Gas Mixtures**

 $PV = ZNR_{\mu}T$ 

$$Z_m = \sum_{i=1}^k y_i Z_i$$

Compressibility factor

 $Z_i$  is determined either at  $T_m$ and  $V_m$  (Dalton's law) or at  $T_m$ and  $P_m$  (Amagat's law) for each individual gas.

Using Dalton's law gives more accurate results.



#### FIGURE 13–8

One way of predicting the P-U-Tbehavior of a real-gas mixture is to use the compressibility factor.









#### FIGURE 13-9

Another way of predicting the P- $\upsilon$ -Tbehavior of a real-gas mixture is to treat it as a pseudopure substance with critical properties  $P'_{cr}$  and  $T'_{cr}$ .

#### Kay's rule

 $Z_m$  is determined by using these pseudocritical properties.

$$P_{\mathrm{cr},m}' = \sum_{i=1}^{k} y_i P_{\mathrm{cr},i}$$

$$T'_{\mathrm{cr},m} = \sum_{i=1}^{k} y_i T_{\mathrm{cr},i}$$

The result by Kay's rule is accurate to within about 10% over a wide range of temperatures and pressures.







Extensive properties of a gas mixture

$$U_{m} = \sum_{i=1}^{k} U_{i} = \sum_{i=1}^{k} m_{i} u_{i} = \sum_{i=1}^{k} N_{i} \overline{u}_{i} \quad (kJ) \quad (13-13)$$
$$H_{m} = \sum_{i=1}^{k} H_{i} = \sum_{i=1}^{k} m_{i} h_{i} = \sum_{i=1}^{k} N_{i} \overline{h}_{i} \quad (kJ) \quad (13-14)$$
$$S_{m} = \sum_{i=1}^{k} S_{i} = \sum_{i=1}^{k} m_{i} S_{i} = \sum_{i=1}^{k} N_{i} \overline{S}_{i} \quad (kJ/K) \quad (13-15)$$

Changes in properties of a gas mixture

$$\Delta U_m = \sum_{i=1}^k \Delta U_i = \sum_{i=1}^k m_i \Delta u_i = \sum_{i=1}^k N_i \Delta \overline{u}_i \quad \text{(kJ)} \quad \textbf{(13-16)}$$
$$\Delta H_m = \sum_{i=1}^n \Delta H_i = \sum_{i=1}^n m_i \Delta h_i = \sum_{i=1}^n N_i \Delta \overline{h}_i \quad \text{(kJ)} \quad \textbf{(13-17)}$$
$$\frac{k}{k} = \frac{k}{k}$$

$$\Delta S_m = \sum_{i=1}^{k} \Delta S_i = \sum_{i=1}^{k} m_i \Delta s_i = \sum_{i=1}^{k} N_i \Delta \overline{s}_i \quad (kJ/K) \quad (13-18)$$









#### **FIGURE 13–11**

The extensive properties of a mixture are determined by simply adding the properties of the components.







Intensive properties of a gas mixture

$$u_m = \sum_{i=1}^k \inf_i u_i$$
 (kJ/kg) and  $\bar{u}_m = \sum_{i=1}^k y_i \bar{u}_i$  (kJ/kmol) (13-19)

$$h_m = \sum_{i=1}^{k} \inf_i h_i$$
 (kJ/kg) and  $\bar{h}_m = \sum_{i=1}^{k} y_i \bar{h}_i$  (kJ/kmol) (13-20)

$$s_m = \sum_{i=1}^k \mathrm{mf}_i s_i \quad (\mathrm{kJ/kg}\cdot\mathrm{K}) \quad \text{and} \quad \overline{s}_m = \sum_{i=1}^k y_i \overline{s}_i \quad (\mathrm{kJ/kmol}\cdot\mathrm{K})$$
(13-21)

$$c_{v,m} = \sum_{i=1}^{k} \underline{\mathrm{mf}}_{i} c_{v,i} \quad (\mathrm{kJ/kg} \cdot \mathrm{K}) \quad \text{and} \quad \overline{c}_{v,m} = \sum_{i=1}^{k} y_{i} \overline{c}_{v,i} \quad (\mathrm{kJ/kmol} \cdot \mathrm{K}) \quad (13-22)$$

$$c_{p,m} = \sum_{i=1}^{k} \underline{\mathrm{mf}}_{i} c_{p,i} \quad (kJ/kg \cdot K) \quad \text{and} \quad \overline{c}_{p,m} = \sum_{i=1}^{k} y_{i} \overline{c}_{p,i} \quad (kJ/kmol \cdot K) \quad (13-23)$$

Properties per <u>unit mass</u> involve <u>mass fractions (mf<sub>i</sub>)</u> and properties per <u>unit mole</u> involve <u>mole fractions ( $y_i$ )</u>.

The relations are exact for ideal-gas mixtures, and approximate for real-gas mixtures.







## **FIGURE 13–12** The intensive properties of a mixture are determined by weighted averaging.







#### **Ideal-Gas Mixtures**

**Gibbs–Dalton law:** Under the ideal-gas approximation, the properties of a gas are not influenced by the presence of other gases, and each gas component in the mixture behaves as if it exists alone at the mixture temperature  $T_m$  and mixture volume  $V_m$ .

Also, the *h*, *u*,  $c_v$ , and  $c_p$  of an ideal gas depend on temperature only and are independent of the pressure or the volume of the ideal-gas mixture.

$$\Delta s_{i} = s_{i,2}^{\circ} - s_{i,1}^{\circ} - R_{i} \ln \frac{P_{i,2}}{P_{i,1}} \cong c_{p,i} \ln \frac{T_{i,2}}{T_{i,1}} - R_{i} \ln \frac{P_{i,2}}{P_{i,1}}$$
(13-24)  
$$\Delta \bar{s}_{i} = \bar{s}_{i,2}^{\circ} - \bar{s}_{i,1}^{\circ} - R_{u} \ln \frac{P_{i,2}}{P_{i,1}} \cong \bar{c}_{p,i} \ln \frac{T_{i,2}}{T_{i,1}} - R_{u} \ln \frac{P_{i,2}}{P_{i,1}}$$
(13-25)

$$P_{i,2} = y_{i,2}P_{m,2}$$
 and  $P_{i,1} = y_{i,1}P_{m,1}$ 









#### **FIGURE 13–13**

Partial pressures (not the mixture pressure) are used in the evaluation of entropy changes of ideal-gas mixtures.







#### **Real-Gas Mixtures**



#### **FIGURE 13–16**

It is difficult to predict the behavior of nonideal-gas mixtures because of the influence of dissimilar molecules on each other.







 $dh_m = T_m ds_m + v_m dP_m$  T ds relation for a gas mixture

 $d(\sum \mathrm{mf}_i h_i) = T_m d(\sum \mathrm{mf}_i s_i) + (\sum \mathrm{mf}_i v_i) dP_m$ 

$$\sum \mathrm{mf}_i (dh_i - T_m ds_i - \upsilon_i \, dP_m) = 0$$

$$dh_i = T_m ds_i + v_i dP_m$$

This equation suggests that the generalized property relations and charts for real gases developed in Chap. 12 can also be used for the components of real-gas mixtures. But  $T_R$  and  $P_R$  for each component should be evaluated using  $T_m$  and  $P_m$ .

If the  $V_m$  and  $T_m$  are specified instead of  $P_m$  and  $T_m$ , evaluate  $P_m$  using Dalton's law of additive pressures.

Another way is to treat the mixture as a pseudopure substance having pseudocritical properties, determined in terms of the critical properties of the component gases by using Kay's rule.









- Composition of a gas mixture: Mass and mole fractions
- *P-v-T* behavior of gas mixtures: Ideal and Real Gases
- Properties of gas mixtures: Ideal and Real Gases



