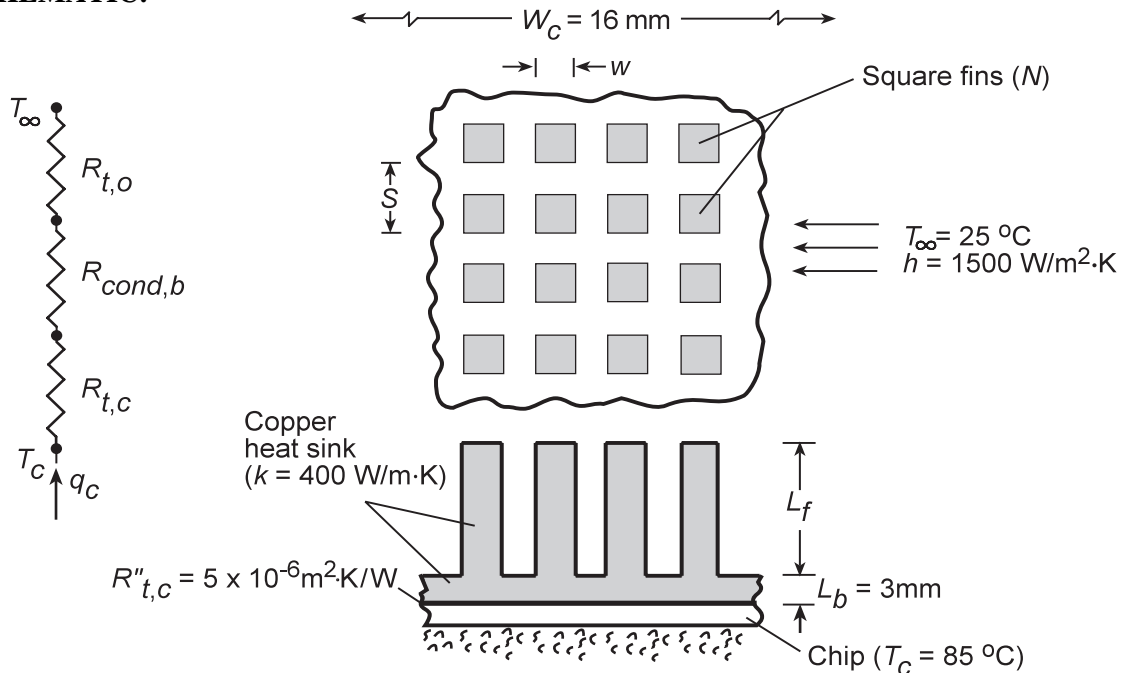


PROBLEM 3.150

KNOWN: Copper heat sink dimensions and convection conditions.

FIND: (a) Maximum allowable heat dissipation for a prescribed chip temperature and interfacial chip/heat-sink contact resistance, (b) Effect of fin length and width on heat dissipation.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state conditions, (2) One-dimensional heat transfer in chip-heat sink assembly, (3) Constant k , (4) Negligible chip thermal resistance, (5) Negligible heat transfer from back of chip, (6) Uniform chip temperature.

ANALYSIS: (a) For the prescribed system, the chip power dissipation may be expressed as

$$q_c = \frac{T_c - T_\infty}{R_{t,c} + R_{cond,b} + R_{t,o}}$$

where $R_{t,c} = \frac{R''_{t,c}}{W_c^2} = \frac{5 \times 10^{-6} \text{ m}^2 \cdot \text{K/W}}{(0.016 \text{ m})^2} = 0.0195 \text{ K/W}$

$$R_{cond,b} = \frac{L_b}{kW_c^2} = \frac{0.003 \text{ m}}{400 \text{ W/m}\cdot\text{K} (0.016 \text{ m})^2} = 0.0293 \text{ K/W}$$

The thermal resistance of the fin array is

$$R_{t,o} = (\eta_o h A_t)^{-1}$$

where $\eta_o = 1 - \frac{N A_f}{A_t} (1 - \eta_f)$

and $A_t = N A_f + A_b = N (4 w L_c) + (W_c^2 - N w^2)$

Continued...

PROBLEM 3.150 (Cont.)

With $w = 0.25$ mm, $S = 0.50$ mm, $L_f = 6$ mm, $N = 1024$, and $L_c \approx L_f + w/4 = 6.063 \times 10^{-3}$ m, it follows that $A_f = 6.06 \times 10^{-6} \text{ m}^2$ and $A_t = 6.40 \times 10^{-3} \text{ m}^2$. The fin efficiency is

$$\eta_f = \frac{\tanh mL_c}{mL_c}$$

where $m = (hP/kA_c)^{1/2} = (4h/kw)^{1/2} = 245 \text{ m}^{-1}$ and $mL_c = 1.49$. It follows that $\eta_f = 0.608$ and $\eta_o = 0.619$, in which case

$$R_{t,o} = \left(0.619 \times 1500 \text{ W/m}^2 \cdot \text{K} \times 6.40 \times 10^{-3} \text{ m}^2 \right) = 0.168 \text{ K/W}$$

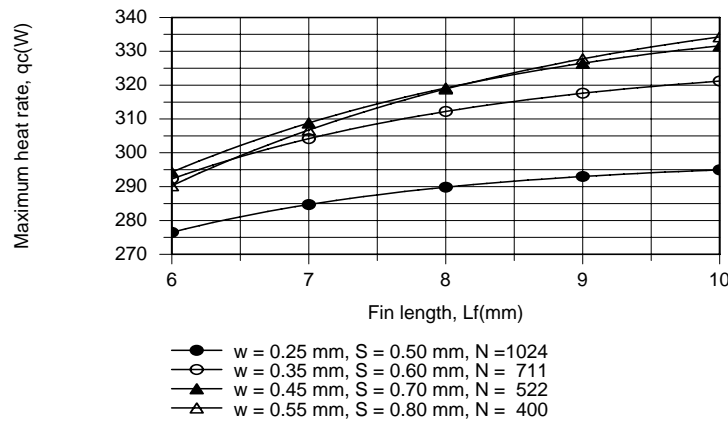
and the maximum allowable heat dissipation is

$$q_c = \frac{(85 - 25)^\circ \text{C}}{(0.0195 + 0.0293 + 0.168) \text{ K/W}} = 276 \text{ W}$$

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(b) The IHT *Performance Calculation, Extended Surface Model* for the *Pin Fin Array* has been used to determine q_c as a function of L_f for four different cases, each of which is characterized by the closest allowable fin spacing of $(S - w) = 0.25$ mm.

Case	w (mm)	S (mm)	N
A	0.25	0.50	1024
B	0.35	0.60	711
C	0.45	0.70	522
D	0.55	0.80	400



With increasing w and hence decreasing N , there is a reduction in the total area A_t associated with heat transfer from the fin array. However, for Cases A through C, the reduction in A_t is more than balanced by an increase in η_f (and η_o), causing a reduction in $R_{t,o}$ and hence an increase in q_c . As the fin efficiency approaches its limiting value of $\eta_f = 1$, reductions in A_t due to increasing w are no longer balanced by increases in η_f , and q_c begins to decrease. Hence there is an optimum value of w , which depends on L_f . For the conditions of this problem, $L_f = 10$ mm and $w = 0.55$ mm provide the largest heat dissipation.